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(54) Title: SILICONE RELEASE LAYERS, LAMINATES AND METHODS

patent), NL (European patent), SE (European patent).

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(57) Abstract

A silicone release laminate formed by a support layer (11) with a silicone release layer (13). A separate pressure-sensitive silicone adhesive layer (12) may be on the same side of the support as the release layer, or on opposite sides of the support. The force required to separate the adhesive from the release layer is less than about 100 grams (3.3 oz.) per inch, and preferably less than 50 grams (1.7 oz.) per inch. The release layer is formed from one or more organopolysiloxanes having a viscosity below 1000 centipoises, and preferably below about 600 centipoises, with a high degree of cross-linking. The organopolysiloxanes may be produced directly by hydrolysis of organo-substituted halosiloxanes and depolymerization; or by hydration of higher molecular weight organopolysiloxanes and heat treatment to produce lower weight constituents.

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SILICONE RELEASE LAYERS, LAMINATES AND METHODS

BACKGROUND OF THE INVENTION

Pressure-sensitive release and adhesive materials are well known and in wide commercial use to secure tapes, labels, or other articles to receiving surfaces. Such adhesives can be attached to a variety of materials by the simple application of pressure. Thus tapes coated with adhesive on opposite sides are used to join two articles together.

Pressure-sensitive adhesives are generally based on elastomeric polymers including natural and synthetic rubbers. They can be compounded with extenders, plasticizers, tackifiers and other materials to provide specifically desired properties. Examples of such materials and their use are provided in numerous prior art U.S. patents, including 3,085,903; 3,246,049; 3,356,635; 3,501,365; and 3,532,652.

Because such adhesives are tacky, it is customary to cover their exposed surfaces temporarily, and removably, with a release layer, typically a nontacky silicone polymer. This facilitates handling, storage and dispensing. The resulting products include label stock in which a base or support is bonded to the adhesive and the exposed adhesive surface is covered with a siliconerelease paper or film. Another example is a spirally wound tape with a film or paper support having one surface bonded to an adhesive. The exposed adhesive surface is in contact with a release layer that is carried by the opposite side of the support, or by a separate interleaving support. Still another example is a spirally wound transfer tape in which the support is coated on both sides with release layers, and one of the release layers is overcoated with adhesive. The adhesive



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initially can be f rmed directly on the support surface, or on th Felease surface. The latter is necessary for transfer tapes with release c atings on both sides of the support. Consistently low uniform release forces between the adhesive and release layer are more difficult to obtain when the adhesive is solidified from a liquid in contact with the release layer surface.

The foregoing structures are "laminates" which are composite structures having at least one support, temporary or permanent, a pressure-sensitive adhesive layer, and at least one release layer in surface contact with the adhesive. Other layers such as a second release layer or a second support may also be present.

Elastomeric, pressure-sensitive silicone adhesives are widely known and have a number of attractive properties. They are useful over a wide range of temperatures, both high and low; they are chemically stable, and have good adhesion to a variety of materials. However, silicone pressure-sensitive adhesives adhere with such tenacity to conventional release surfaces, that the materials often tear before releasing. The consequence is that the use of silicone adhesive has been limited generally to direct application without a release layer, or to use with plastic films strong enough to withstand the considerable release forces required in unwinding spiral tapes. Release surfaces with ridges which tend to reduce contact area have also been employed with limited success, but at increased expense.

Accordingly, an object of the invention is to realize a silicone pressure-sensitive release laminate that is practical for use, both immediately after preparation and after extended periods of storage.

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Another object is t realize silicone adhesive laminate trustures which can be releasably separated with stripping or release forces c mparable with known, nonsilicone pressure-sensitive adhesive laminates.

Still another object is to realize silicone pressuresensitive laminate structures which permit the use of existing pressure-sensitive application techniques and equipment.

A further object of the invention is to facilitate the use of silicone adhesives. A related object is to provide release materials for such adhesives which expedite their use.

Still another object is to achieve release and adhesive combinations which are readily produced and are usable over a wide range of temperature conditions. A related object is to achieve a silicone release and adhesive laminate which is operable under frigid Arctic conditions, as well as humid and high temperature tropical conditions.

SUMMARY OF THE INVENTION

In acc mplishing the foregoing and related objects, the invention provides for the mpl yment of one or more releasable dimethylpolysiloxanes which, before curing, have viscosities in the range from about 60 centipoises to about 100 centipoises, and from about 100 centipoises to about 600 centipoises. A less preferred range of viscosities is from above about 600 centipoises to below 1000 centipoises. A similarly suitable viscosity range extends below about 60 centipoises.

Silicone release resins for the practice of the invention are sold essentially as linear polymers or prepolymers in liquid form, with or without solvents. They are coated onto paper, film or other supports and then cured, typically by heat and/or surface catalytic action, to form solid, nontacky, cross-linked polymers in situ.

These release resins are formed from halosilanes and consist predominantly of repeating units of the structure

where R is hydrogen or a hydrocarbon radical, principally a lower alkyl or aryl, typically methyl;

- 0 is oxygen: and
- Si is silicon.

The degree of polymerization is such as to produce a liquid linear prepolymer material with no significant cross-linkage. While liquids are preferred, high molecular weight wax-like solids can be substituted where sufficient solvent or can be employed to provide fluidity for coating without premature curing.

It is b lieved that presently known silicone linear release prepolymers consist f at least 95 per cent repeating units f the above structure with reactive end groups, but that small quantities of other modifying units may be present, if desired. Such release materials are described, for example, in an article by Alvin E. Bey, titled "New Developments in Silicone Release Coatings for Pressure-Sensitive Adhesives", in the October, 1972 issue of Adhesives Age, pages 29-32.

In accordance with the present invention, it has been found that silicone pressure-sensitive adhesives can be contacted with release layers formed from selected silicone release polymers, stored for extended periods, and removed for use when needed. The equipment and forces are generally comparable to those heretofore employed with rubber and acrylic-based adhesives. These results are obtained by employing one or more silicone release polymers with a net viscosity below 1000 centipoises, which subsequently are highly cross-linked. The degree of cross-linking can be conveniently measured by the absorption of solvent. The greater the degree of crosslinking, the less is the absorption of solvent. Silicone release polymers are sufficiently cross-linked for use with the laminates of the present invention if they absorb less than about 200 per cent of their cured weight of the solvent heptane.

The absorption of heptane is measures as follows: A sample of liquid coating material, catalyzed for curing, is placed in a container from which it can be removed after curing. The container may be a small laboratory weighing dish of aluminum foil. Inert solvent, if present, is then removed and the liquid fully cured. A sufficient sample should be used to provide a cured thickness of about one fourth inch. The cured sample is then removed, weigh d, and immersed in heptane until

the sample reaches substantially constant weight. The sample is removed fr m the heptane, the surface dried by blotting and the sample is reweighed. The increase in weight represents the amount of absorbed heptane.

When measured by the foregoing technique, it has been found that conventional silicone release polymers will absorb about 600 per cent or more of their original weight and that the increase in weight often continues well beyond twenty-four hours. Preferred materials according to the present invention usually attain substantially constant weight within twenty-four hours.

The release mechanism has been previously theorized, for example, in Bey, cited above, as involving a low polarity surface of low surface tension, highly flexible polymer chains, incompatibility of the release surface with dissimilar contacting adhesive polymers. The degree of cross-linking affects the release forces. However, such theories have not led to successful release laminates for silicone pressure-sensitive adhesives.

Surprisingly, and in accordance with the present invention, it has been discovered that if the degree of cross-linking is substantially increased over prior practice, laminates with silicone adhesives can be obtained with low release values even though the flexibility of the release polymer is reduced and the polymeric materials in contact have substantial similarity.

A variety of chemical techniques are known for obtaining a high cross-link density. For example, a high degree of functionality can be provided on a polysilox-ane prepolymer, as by silicon-bonded hydrogen or vinyl substituents, which are p lymerized and cross-linked with

polyfunctional cross-linking agents. Additive reactions between unsaturated hydrocarbon groups, such as vinyls or the like, and silic n-bonded hydrogens are preferred. The unsaturated hydrocarbon groups may be provided as reactive groups in a hydrocarbon molecule, preferably of low molecular weight, as in Example I, or on a polysiloxane prepolymer, as in Example VI, below.

It is also preferred that all or a majority of the polysiloxane prepolymers be of low molecular weight, preferably having a Brookfield viscosity at 25°C. below 1000 centipoises, corresponding to a molecular weight below about 25,000. Such lower molecular weight prepolymers are believed to minimize steric effects in the attainment of a highly cross-linked structure. The total liquid coating prepolymer composition, absent inert solvent, preferably has a viscosity below about 600 centipoises and most preferably less. Particularly suitable materials have a net viscosity in the range extending from 300 to between 60 and 100 centipoises. Less suitable but usable are materials having a viscosity range above 600 centipoises and below 60 centipoises.

It is preferred in some cases that the silicone release layers of the present invention be formed from reactive polysiloxane prepolymer compositions having a substantial content of silicon-bonded hydrogen substituents sufficient to provide an infra-red (IR) absorption ratio above about 0.4 for the ratio of (a) silicon-hydrogen (Si-H) absorption, in the range from about 4.5 to 4.8 microns, to (b) for carbon-hydrogen (C-H) absorption in the range from about 3.0 to 3.5 microns.

Even where the absorption ratio for hydrogen-bonded silicon is below 0.4, suitabl releas materials can be realized if the material contains a sufficient number of other reactive groups, such as vinyls.

Prepolymers containing silicon-bonded hydrogen can comprise the major component, as in Examples I-V, below, which can be highly cross-linked with co-reactive silanes, multivinyl containing cross-linking agents, or similar reactive unsaturated compounds such as dicyclopentadiene, or, as illustrated in Example VI, the silicon-bonded, hydrogen-containing prepolymer can be employed to cross-link other co-reactive polysiloxane prepolymers having sufficient co-reactive substituents, preferably vinyl groups, to provide a siloxane copolymer with a high degree of cross-linking. Catalysts for the above reactions are known and are exemplified in the Examples.

DESCRIPTION OF THE DRAWINGS

In the accompanying drawings:

Figure 1 is an infrared (IR) spectrographic absorption chart for silicone release resin prepolymer No. 4280 of the General Electric Company;

Figure 2 is an IR spectrographic absorption chart for silicone release resin prepolymer No. SS4281C of the General Electric Company;

Figure 3 is an IR spectrographic absorption chart for silicone release resin prepolymer No. 4191 of the General Electric Company;

Figure 4 is an IR spectrographic absorption chart for silicone release resin prepolymer No. X2-7018 of the Dow Corning Corporation;

Figure 5 is an IR spectrographic absorption chart for silicone release resin prepolymer No. X2-7016 of the Dow Corning Corporation:

Figure 6 is an IR spectrographic absorption chart for silicone release resin prepolymer No. 23/30 of the Dow Corning Corporation;

Figure 7 is an IR spectrographic absorption chart for silicone release resin prepolymer No. EP 6396 of the Imperial Chemical Industries, Ltd., Stevenston, Ayrshire, Scotland;

Figure 8A is an IR spectograph absorption chart for Dow-Corning Q-2-7044/7045;

Figure 8B is a reduced portion of Figure 8A to permit determination of the IR ratio;

Figure 9A is a schematic diagram of a laminate in accordance with the invention;

Figure 9B is a schematic diagram of another laminate in accordanc with the invention; and

Figure 9C is a schematic diagram of a further laminate in acc rdance with the invention.

DETAILED DESCRIPTION

Detail d considerations applicable to the practice of the invention are set f rth below

(a) Absorption Spectra

The absorption spectra of Figures 1-8 were obtained by placing a cast film, free of solvent, in or on a sodium chloride capillary cell or plate. Cells were used for lower viscosity materials where too little material was retained on a plate (Figures 2, 4, 5 and 7). Plates were used for higher viscosity materials (Figures 1, 3 and 6). The runs were performed on an INFRACORD prism IR spectrophotometer. The cast film was of a thickness such that both absorption peaks of interest, when present, fell within about the absorption region extending from above 0.2 to 0.7.

The determination of the ratio of absorption in the range from 4.5 to 4.8 microns for silicon-bonded hydrogen (SiH), to the absorption in the range from 3.0 to 3.5 microns for the carbon-bonded hydrogen (CH) is illustrated with respect to Figure 7 as follows:

- (a) The first absorption peak is 0.72 at 3.4 microns. The estimated base line at 3.4 microns is about 0.05 (by straight line extrapolation across the absorption interval indicated by the broken line).
 - (b) The absorption at 3.4 microns for (CH), was therefore determined to be about 0.67 (0.72 minus 0.05).
- (c) Similarly, the second absorption peak was 0.29 at 4.6 microns. The absorption (SiH), adjusted for base line was determined as 0.275 (0.29 minus 0.015).
- (d) The ratio (IR), therefore was 0.41 (obtained from dividing 0.275 by 0.67). (IR)₁ = $(SiH)_1/(CH)_1$

. IR ratios from Figures 1-8 were calculated as indicated above and are listed in the following TABLE I.

(IR Ratios)

TABLE I

F1gure	Numerator (S1H) Absorption (4.5-4.8)	Denominator (CH) Absorption (3.0-3.5)	S1H/CH Absorption Ratio
1	*****	0.19	
2	0.65	0.43	1.51
3	0.05	0.20	0.25
4		0.47	
5	0.34	0.43	1.03
6	0.17	0.72	0.24
7	0.27	0.67	0.41
8	0.13	0.57	0.23

As sold commercially and recommended for use by the suppliers, the prepolymers of Figures 1 and 2, and also of Figures 4 and 5, are mixed in the proportion of 10 parts by weight of the first material to 1 part by weight of the second material and coated with or without solvent, and cured. They form release layers, but not for silicone adhesives.

The materials of Figures 3 and 6 are conventional 'solvent coating release materials, cured with catalyst and small quantities of reactive silanes as recommended by the suppliers.

The material of Figure 7 is a solventless coating material ured with added platinic acid catalyst containing dicyclopentadi ne, as recommended by the supplier.

When such materials are coated on densified release paper, cured, and laminated to conventional rubber or acrylic-based pressure-sensitive adhesives, suitably stable release forces are generally obtained for solvent applied release layers in the range of 16 to 40 grams per inch of width at slow speed, and 40 to 100 grams per inch of width at high speed, measured as more fully explained in Example 1 below.

The coatings applied without solvents generally give about one-half these values. However, when laminated to silicone-based pressure-sensitive adhesives, especially after a few days of storage, conventional release sheets often tear before release is obtained. Also, the tack or adhesion of the silicone adhesives is sometimes diminished, believed to be due to retention of release polymer on the surface of the adhesive.

In the case of Figure 8, although the absorption ratio of silicon-bonded hydrogen is low (less than 0.40), there are compensating vinyl reactive groups which make use of material suitable for the practice of the invention.

(c) Preferred embodiments of the Invention

The invention is illustrated by the following nonlimiting examples:

13 EXAMPLE I

A carrier was provided by a conventional 42-pound per ream (250,000 square inches) super calendered and densified Kraft release paper and coated as follows:

A silicon-release polymer EP 6396 from Imperial Chemical Industries Limited (ICI), Ayrshire, Scotland was mixed with ICI catalyst EP 6439 (platinic acid type containing dicyclopentadiene) in the weight ratio of 1.5 parts catalyst to 100 parts resin and placed in the pan of an offset gravure coating apparatus. EP 6396 is believed to be predominantly silanol terminated polydimethylsiloxane having a viscosity of 60 to 100 centipoises at 25°C., in combination with a minor proportion of polymethylhydrogensiloxane having a viscosity of about 25 centipoises at 25°C. The net viscosity is about 70 centipoises and is verifiable from the IR spectrographic absorption chart of Figure 7. addition Figure 7 and Table I show that the material has a sufficient amount of hydrogen-bonded silcicon (IR ratio of 0.45) to provide an adequate release.

A gravure roll, partially immersed in the pan, with 150 lines per inch engraved on steel was employed with a rubber transfer roll operated at a roll speed ratio of 1:1. The release carrier paper was fed over the transfer roll by a steel drive roll, with the paper fed between the nip formed by the rubber transfer roll and the steel drive roll, at a speed six times as great as the linear speed of the surface of the transfer roll surface. This provided a smooth, uniform coating of about 0.3 pounds coating per

ream. The coating was then passed into a hot air oven and cured for 7 seconds at 395°F (202°C). The second or reverse side was then similarly coated and cured, with the fir t side again heated for 7 seconds at 395°F (202°C).

The release paper was then further coated on the first, twice heated side, by drawing the paper under a shimmed steel bar with 1.0 to 1.5 mils thickness of silicone pressure-sensitive adhesive (after drying and curing). The adhesive employed was SR 574 obtained from the General Electric Company and catalyzed as recommended with 1.5 per cent by weight of equal weight parts of dichlorobenzoyl peroxide and silicone oil or dibutyl phthalate. The coating was cured at 300°F. for 2 minutes. The cured adhesive was covered with a 0.002 inch thick strip of Mylar polyester film and a compressive force of about 400 pounds per inch applied for eight minutes.

It is to be noted that the composition for SR 574 adhesive is disclosed by William J. O'Malley in an article titled "Silicone Pressure Sensitive Adhesives for Flexible Printed Circuits", April 24, 1974, prepared for a meeting of the Multilayer Committee of the Institute of Printed Circuits. The specific composition of SR 574 is discussed, for example, on page 1 at line 8 and in Figures 1 and 2. It is indicated that pressure sensitive adhesives of the SR 574 type are based on the combination of a gum and an "MQ" resin. The gum component, as shown by Figure 1 of the article, is a polysiloxane gum such as methylphenylpolysiloxane. Figure 2 of the article discloses the MQ resin to be an organopolysiloxane resin.

In addition the preparation of organopolysiloxane pressure sensitive adhesives is specifically set forth in U.S. Patent 2,857,356 to Goodwin, Jr., which teaches that specific resins (column 4, beginning at line 15) are reacted with linear, high-viscosity organopolysiloxane fluids (column 4, beginning at line 47).

Slow speed release between the silicone adhesive and the silicone release surface was measured with an Instron tester, Model TM. In the slow speed test, a sample 1/2 inch wide by six inches in length was stripped at 900 and 12 inches per minute and the release measured. This procedure is a modification of TLMI Adhesion Test No. VII-LD. In the modified procedure the sample to be tested is secured to a rigid plate using two-sided adhesive tape, with both release layer and its carrier exposed. Removal of release layer is initiated, and the sample is clamped in the jaws of the tester.

For high speed stripping, the test was conducted on a TLMI tester, and samples 1 inch by 6 inches were stripped at 180° and 600 inches per minute, following TLMI release test method VIII-LD270. the measured stripping or release forces were as follows, for various periods of storage time at standard conditions of temperature and pressure following preparation of the laminate:

Storage Interval	Low Speed Release Force	High Speed Release Force		
Zero	9-16 grams	25-30 grams		
24 hours	14-24 grams	25-30 grams		
1 week	15-25 grams	25-30 grams		

16 EXAMPLE II

Ten grams of ICI release prepolymer EP 6396 was dissolved in 87 grams of heptane. To this solution was added one (1.0) c.c. of a 50 per cent by weight solution of triacetoxy methyl silane in toluene, and 0.5 grams of di-N-butyl tin dioctoate, a known silicone catalyst.

The resulting release mixture was coated using a Number 4 Mayer rod onto a support film of Mylar polyester, dried and cured in an oven for 20 seconds at 275°F.

When overcoated with General Electric SR 574 silicone pressure-sensitive adhesive, laminated and tested, all as set forth in Example I, low release values immediately and after storage for one week were obtained.

When the release mixture was coated on untreated paper low release values were not obtained. However, if the paper is provided with a suitable barrier coating, e.g. a conventional cured silicone release coating such as the materials of Figures 3 or 6, paper can be used as the support.

EXAMPLE III

General Electric experimental pressure-sensitive adhesive No. 404-333 was substituted for adhesive SR 574 in Example I. The resulting material was laminated and tested as in Example I. Similar release values were obtained.

EXAMPLE IV

The prepolymer of Figure 2, having a comparatively high IR absorption ratio (of 1.51 as shown in Table I) and a viscosity of 600 centipoises, is used after being suitably cured with catalyst such as that of Example I. The viscosity of 600 centipois s is verifiable from literature supplied by the manufacturer. Impr ved release properties f r silicone adhesives are obtained.

17 EXAMPLE V

The prepolymer of Figure V also having a comparatively high IR absorption ratio (of 1.03 as shown by Table I) and a viscosity believed to be below 1000 centipoises is used when suitably cured with a catalyst such as that of Example I. The low viscosity below about 1000 centipoises is supported by the suitability of the material for reverse roll coating. Improved release properties for silicone adhesives are obtained.

EXAMPLE VI

A mixture of one part by weight Q-2-7045 was mixed with ten parts Q-2-7044, obtained from the Dow Corning Corporation. The mixture was substituted for the ICI material specified in example I.

Q-2-7044 is understood to be a polysiloxane having a plurality of reactive vinyl substituents attached to its silicone atoms, a viscosity of about 300 centipoises, and a molecular weight of about 15,000, corresponding to a degree of polymerization of about 200. It also contains rhodium, or platinum-based catalyst.

Q-2-7045 is understood to be approximately 60 per cent by weight Q-2-7044 and 40 per cent by weight polymethylhydrogensiloxane of low molecular weight. This material is understood to have a degree of polymerization of about 40 units and an IR ratio substantially greater than 0.4. The reactive hydrogen substituents of the Q-2-7045 cross-link with the vinyl groups of the Q-2-7044 prepolymer.

The material was coated, cured, and tested in acc rdance with Example I, except that the rubber transfer roll and the steel drive roll were driven at the same speed. This was greater than the surface speed of the gravure roll by 10 per cent or more. A coating weight of between one and two pounds per ream was applied.

Although this material has a comparatively low absorption ratio (of 0.20 as indicated in Table I) it has a sufficient number of reactive vinyls to provide a suitable release.

Similar results were obtained as for Example I. addition this release material was employed on the Alaska pipeline and found to be the only material, of those tested, that could be used successfully under Arctic conditions.

(d) Summary of the Examples

Of the foregoing Examples I, III, IV and VI are preferred. Assurance of the suitability of the material is made by choosing relatively low viscosity material below 1000 centipoises at 25°C, and preferably lower, with a sufficient number of reactive groups, either at or intermediate terminal positions. In the case of reactive hydrogen an indicator of suitability is given by a relatively high IR ratio (above 0.4). Other indices of active sites are employed for vinyls, alkoxys, esters and the like.

(e) Preferred Adhesives

It is also preferred to use a pressure-sensitive silicone adhesive containing an appreciable number of essentially

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inert substituents other than methyl, for example phenyl groups, as disclosed, for example, in U.S. Patents 2,857,356 and 3,839,075. Such groups may be provided, for example, by incorporating phenyl-methyl siloxane in the polymer monomer units. Inclusion of "M" and "Q" units as described in the above patents is also preferred. The amount of such "M" and "Q units can be varied to vary the tack of the resulting adhesives.

(f) Laminates According to the Invention

For each of the above Examples, the pressuresensitive laminates were in accordance with Figure 9A.
Each such laminate 10 consisted of a support layer 11 of
Mylar film or tape; a silicone pressure-sensitive
adhesive layer 12 adhered to one surface of the film 11;
a cured, highly cross-linked silicone release polymer
layer 3 removably adhered upon the adhesive layer; and a
release paper carrier 14 adhered to the release layer on
the side opposite the adhesive. The adhesive can be
readily stored, handled, dispensed and applied in this
form.

To form a spirally-wound tape 10' as illustrated in Figure 8B, the silicone release layer 12 is applied to the side of the Mylar film 11 opposite the adhesive 13 and no separate carrier sheet is needed.

For a transfer tape 10" as illustrated in Figure 9C, both sides of the Mylar 11 or other support are coated with respective release layers 12 and 12'. It should be noted that low release values were obtained even though the adhesive was applied and cured directly on the release surface.

(g) Cross-Linking Considerations

Each of the foreg ing Exampl s provides a high degree of cross-linking. In all cases polysiloxane prepolymers with a plurality of silicon-bonded hydrogen substituents were cross-linked with compounds having a plurality of vinyl, hydroxyl or esteryl groups that are co-reactive with the hydrogen substituents. The prepolymers are believed to have substantially the following structure:

where R' is an alkyl, preferably methyl, radical;

- R is partially or entirely hydrogen and the balance if any, is an alkyl, preferably lower carbon chain radical;
- O is oxygen;
- Si is silicon; and
- X is below about 350 and preferably less.

 Such low molecular weight material provide a Brookfield viscosity at 25°C. below 1000 centipoises, and/or preferably less. These prepolymers are believed to be substantially homopolymers of methylhydrogenpolysiloxane when X is about 40; or are copolymers with dimethylpolysiloxane when X is greater than 40 and below about 350 and preferably below about 300.

The above prepolymers, suitably catalyzed, are copolymerized and highly cross-linked by materials having a plurality of groups that are co-reactive with the hydrogen substituents. Table III, below, summarizes the, cross-linking materials employed in the Examples:

21 TABLE III

Cross-linker Examples

- (1) disilanol terminated I, II, IV and
- (2) dicyclopentadiene I, III, IV and V
- (3) methyl-triacetoxy silane II
- (4) polysiloxane prepolymers VI having a plurality of vinyl substituents VI

The organopolysiloxanes of Example VI and Table III (4), above, are believed to have substantially the following formula:

where R' is an alkyl, principally methyl radical;

R" is a mixture of vinyl and lower alkyl groups;

- 0 is oxygen;
- Si is silicon; and
- Y is below about 350 and preferably below 30.

Organosiloxanes should comprise the major portion of the coating composition. Where hydrocarbon cross-linking agents such as dicyclopentadiene are used, they preferably have small structures and are used in limited amounts sufficient to provide highly cross-linked organosilicone.

Where co-reactive polysiloxane prepolymers are employed, the ratio may vary considerably provided sufficient quantities of each reactive group are employed to produce a dense, highly cross-linked silicone. Thus in Example VI a minor portion of a silicon-bonded hydrogen-containing prepolymer is employed with a substantial

number of reactive hydrogen substituents. Undue stoichiometric xcess of unreacted silicon-bonded hydrogen substituents is preferably av ided.

It is also known that hydroxyl and alkoxy groups are co-reactive with silicon-bonded hydrogen polysiloxane substituents.

(h) Cure Considerations

Cure of the release coatings should be carried substantially to completion, so that low release values are obtained. A minimum of free reactive groups at the surface is considered desirable. Substantially complete cure can be achieved using sufficient heat and time, e.g. from about 7 to about 20 seconds at 395°F. or higher. Infra-red heaters can be employed usefully at the end of the cure cycle, for example to raise the coating temperature momentarily to about 500°F.

(1) Conversion of Surface Reactive Groups

Where initial release values are too high, improvement can sometimes be provided by chemically converting free surface reactive groups to more inert groups. For example, free surface Si-H groups may be treated with hydrogen free, reactive silanes such as by a gas phase exposure to a mixture of trichloromethylsilane and dichlorodimethyl silane for 5 seconds at 225°F., or a liquid treatment with a 3 per cent by weight solution of trimethoxymethyl silane in heptane, with di-N-butyl tin diacetate as catalyst, followed by drying. Curing with sufficient heat is desirable.

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Control of moisture during cure may also be important in obtaining low release values, especially for low coating weights. Ambient moisture in the drying and curing air has not been a problem and reasonable care in excluding contamination or condensation of water in the coating prepolymer mixture is sufficient. However, excess moisture in the carrier paper, where used, can be troublesome, and it is preferred that the paper have a moisture content by weight of about 4 per cent or less. Pre-drying can be employed, if necessary.

(j) Coating Techniques

Good coating technique is desirable, with sufficient coating material applied to obtain a smooth uniform surface with preferably between about 0.2 and 2.0 pounds of cured release coating per ream. Coating weights between about 1.0 and 2.0 pounds per ream are preferred. These coating weights are used for normal support having good hold-out surfaces. Higher amounts may be required when the liquid release materials are applied to more porous surfaces to compensate for absorption into the support.

High speed release forces are often more important. than low speed release because of the common use of high speed applicating equipment. High speed release forces less than about 100 grams (3.3 ozs.) per inch of width are preferred, forces less than about 50 grams (1.7 ozs.) are more preferred, and about 25 grams (0.8 oz.) or less per inch of width are most preferred. Such low values have

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not been obtainable previously in consistent c mmercial practice prior to the present invention, especially where the adhesive c ating is form d directly on the release surface. Low release values are particularly important amounts may be required when the liquid release materials are applied to more porous surfaces to compensate for absorption into the support.

High speed release forces are often more important than low speed release because of the common use of high speed applicating equipment. High speed release forces less than about 200 grams per inch of width are preferred, forces less than about 100 grams are more preferred, and about 50 grams or less per inch of width are most preferred. Such low values have not been obtainable previously in consistent commercial practice prior to the present invention, especially where the adhesive coating is formed directly on the release surface. Low release values are particularly important where paper is used as a carrier due to its limited strength, and where high speed applicating equipment is used.

(k) Sources of Release Polymers

The release polymers used in the Examples were obtained from the commercial sources indicated. Other release polymers of suitable viscosity and absorbance can be produced by hydrolysis of organo substituted halosilanes. This results in a hydrolyzate of linear and cyclic polysiloxanes. The hydrolyzate is treated with a catalyst, such as potassium hydroxide, to bring about depolymerization. The desired polymers are separated by distillation.

Suitabl organopolysiloxane can als be produced by hydration of high order rganopolysiloxanes and heating. This causes the high rder rganopolysiloxane to break into low order materials. For example, an organopolysiloxane with a viscosity of 1,000,000 centipoises at 25°C may be heated at 160°C with 1.0 per cent by weight water for 2 hours to reduce the material to chains having viscosities below 1000 centipoises.

It will be understood that the foregoing description is for illustration only and that the invention includes all modifications and equivalents within the scope of the appended claims.

WHAT IS CLAIMED IS:

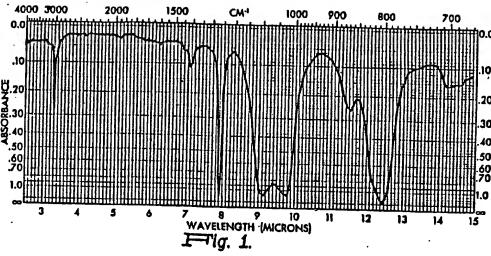
- 1. An article comprising a backing, and a releasable organopolysiloxane on said backing, said organopolysiloxane having a viscosity before curing below 1000 centipoise at 25°C.
- 2. An article as defined in claim 1 wherein the releasable material can contain vinyl groups prior to curing, which vinyl groups can be alkylvinylsiloxy; the releasable material can contain reactive hydrogen prior to curing, which reactive hydrogens can be alkylhydrogensilanol; and the releasable material can be dimethylpolysiloxane cured into a dense polymer.
- 3. An article as defined in claim 1 wherein said viscosity is in the range from about 60 centipoises to about 600 centipoises.
- 4. An article as defined in claim 1 wherein an adhesive is positioned on said backing which adhesive can comprise the intercondensation product of a mixture containing an organopolysiloxane resin and at least one alkylaryl polysiloxane gum.
- 5. An article as defined in claim 1 wherein said releasable organopolysiloxane, before curing, is formed from a plurality of prepolymers having a viscosity below 1000 centipoises.
- 6. An article comprising a backing and a releasable organopolysiloxane on said backing having an absorption ratio greater than 0.4 for hydrogen-bonded silicon; less than 4.0 when the releasable material contains vinyl hydroxyl or ester groups; and the releasable organopolysiloxane layer can be cross-linked to absorb less than 200 percent of its cured weight in solvent.

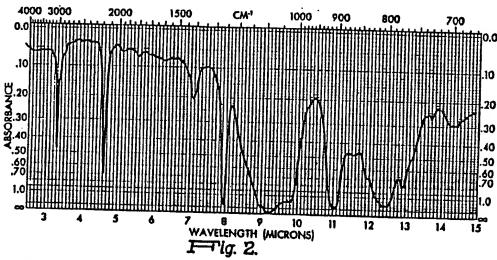
7. An article as defined in claim 1 wherein said organopolysiloxane has the following structure

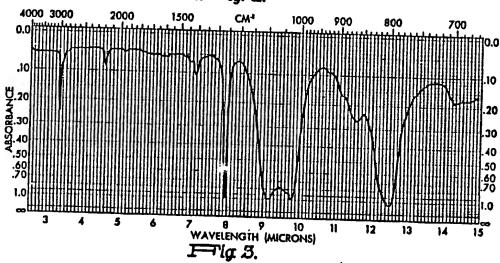
Where R' is an alkyl, preferably methyl radical;

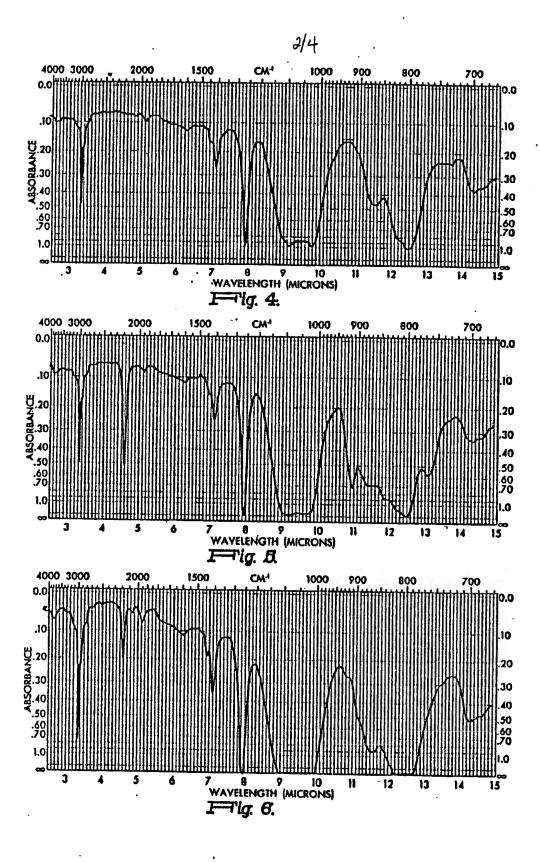
- R is partially or entirely hydrogen, partially vinyl, and/or partially hydroxyl, with the remainder alkyl;
- O is oxygen;
- Si is silicon; and
- X is below 350 and preferably below 300.
- 8. The method of producing the article of claim 1 comprising the steps of
- (a) coating the releasable organopolysiloxane on said backing; and
- (b) curing the releasable polysiloxane on said backing; which steps can be supplemented by the following further steps:
- (c) applying an organopolysiloxane pressure-sensitive adhesive layer directly to said backing or upon said releasable siloxane; and
 - (d) curing said adhesive on said backing.
- 9. The method of claim 8 further including the step of converting residual surface reactive groups to more inert groups, which surface groups can be treated with hydrogenfree, reactive silanes.
- 10. The method of claim 8 wherein a catalyst is used slected from the class consisting of
 - (a) di-n-butyltindiesters;
 - (b) rhodium complexes; and
- (c) platinum complexes; and a cross-linker can be used selected from the class consisting of
 - (a) dicyclopentadiene,
 - (b) methyltriacetoxysilane
 - (c) polysiloxanes with a plurality of vinyl substitutes;
 - (d) disilanol terminated dimethylpolysiloxanes.

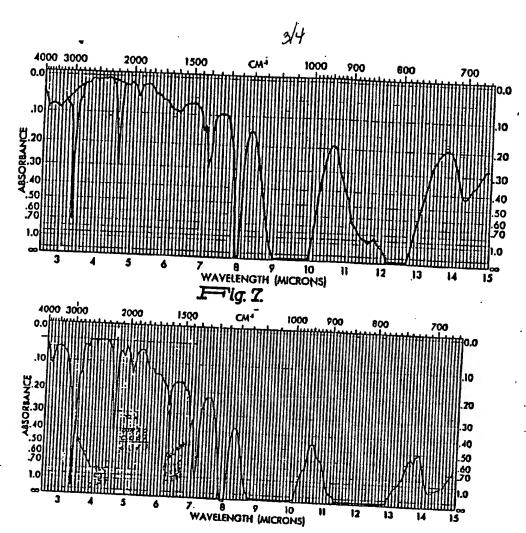


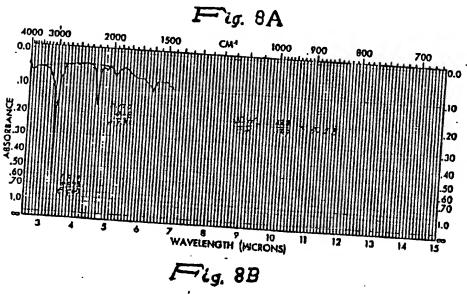












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Fig. 9A

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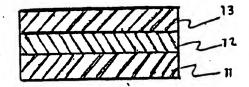


Fig. 9B

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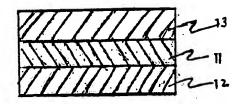
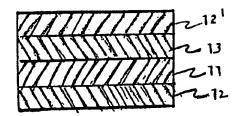


Fig.9C

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INTERNATIONAL SEARCH REPORT

International Application No PCT/US85/02424

I. CLASSIFICATION F SUBJECT MATTER (if several classification symbols apply, indicate all) *								
According to International Patent Classification (IPC) or to both National Classification and IPC								
INT. CL.4 B32B 7/26; 600 7/02 U.S. CL. 427/154, 208.4; 428/40, 352, 354, 447								
11. FIELDS SEARCHED								
			1	Ainimum Documen	tation Searched	+		
Classification	on System				Classification Sy			
U.S. 427/154, 155, 208.4, 208.8; 428/40, 352, 354, 355, 447								
				n Searched other ti t such Documents				
III. DOCL	JMENTS C	ONS	DERED TO BE REL	EVANT 14				
Category •	Citatio	on of	Document, 16 with ind	ication, where appr	opriate, of the r	elevant	passages 17	Relevant to Claim No. 18
Y	US,	Α,	2,985,554	(AVERY A 23 MAY 1		PRO	DUCTS)	1-10
Y	US,	Α,	3,006,463	(MINNESO FACTURIN 1961				1-10
Y	US,	Α,	4,039,707	(GENERAL 02 AUGUS		IC C	0.)	1-10
Y	US,	Α,	4,313,988	(MINNESO FACTURIN 1982				1-10
Y	US,	Α,	4,347,346	(GENERAL 31 AUGUS	ELECTR	IC C	0.)	1-10
Y	US,	Α,	4,386,135	(MINNESO FACTURIN	TA MINII G CO.)	NG &	MANU- MAY 1983	1-10
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*Special categories of cited documents: 15 "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date and not in conflict with the application but cited to understand the principle or theory underlying the invention "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "I" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to understand the principle or theory underlying the or priority date and not in conflict with the application but cited to underst								
IV. CERTIFICATION Date of the Actual Completion of the International Secret 1.								
Date of the Actual Completion of the International Search 2 O3 MARCH 1986 Date of Mailing of this International Search Report 3 O 7 MAR 1986								
Internation	International Searching Authority 1 Signature of Authorized Officer 10							
ISA/US				W.J. VanBalen				